

1 **TITLE**

2 CAERvest® – A novel endothermic hypothermic device for core temperature cooling – Safety
3 and efficacy testing

4 **RUNNING TITLE**

5 CAERvest® core temperature cooling

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17 **ABSTRACT**

18 Introduction: Cooling of the body is used to treat hyperthermic individuals with heatstroke or to
19 depress core temperature below normal for neuroprotection. A novel chemically activated,
20 unpowered cooling device, CAERvest[®], was investigated for safety and efficacy, with the
21 feedback used to inform device development.

22 Methods: Eight healthy male participants (body mass 79.9±1.9kg and body fat percentage
23 16.1±3.8%) visited the laboratory (20°C, 40% RH) on four occasions. Following 30min rest,
24 physiological and perceptual measures were recorded. Participants were then fitted with the
25 CAERvest[®] proof of concept (PoC), prototype 1 (P1), 2 (P2) or 3 (P3) for 60min. Temperature,
26 cardiovascular and perceptual measures were recorded every 5min. After cooling, the
27 CAERvest[®] was removed and the torso was checked for cold-related injuries.

28 Results: Temperature measures significantly ($p<0.05$) reduced pre-to-post in all trials. Larger
29 reductions in *core* and *skin temperature* were observed for PoC (-0.36±0.18 and -1.55±0.97°C)
30 and P3 (-0.36±0.22 and -2.47±0.82°C), compared to P1 and P2. No signs of cold-related injury
31 were observed at any stage.

32 Conclusion: This study demonstrates the CAERvest[®] is an effective device for reducing body
33 temperature in healthy normothermic individuals without presence of cold injury. Further
34 research in healthy and clinical populations within controlled and field-settings is warranted.

35 **Key Words**

36 Thermoregulation; Hyperthermia; Heat related illness; Cooling; Targeted temperature
37 management

38

39	Abbreviations
40	Δ change
41	ANOVA analysis of Variance
42	BP blood pressure
43	BMI body mass index
44	BSA body surface area
45	CBT core body temperature
46	CPR cardiopulmonary resuscitation
47	CV coefficient variation
48	CWI cold water immersion
49	<i>HR</i> heart rate
50	HRI heat related illnesses
51	<i>M</i> mean
52	NBM nude body mass
53	ηp^2 partial eta squared
54	PoC proof of concept
55	P1 prototype 1
56	P2 prototype 2
57	P3 prototype 3
58	ROSC return of spontaneous circulation
59	<i>SD</i> standard deviation
60	TEM typical error of measurement
61	T_{arm} arm temperature
62	T_{calf} calf temperature
63	T_{chest} chest temperature
64	T_{thigh} thigh temperature
65	T_{re} core temperature
66	TSS thermal sensation
67	T_{skin} skin temperature
68	TTM targeted temperature management
69	U_{osm} urine osmolality
70	U_{sg} urine specific gravity
71	
72	

73 **1.0 INTRODUCTION**

74 Active cooling treatment is used to reduce an abnormally or dangerously elevated core body
75 temperature (CBT), as in heat related illnesses (HRI). It may also be used to reduce a patient's
76 CBT below normal (e.g. targeted temperature management [TTM]) during cardiac surgery and
77 as neuroprotective treatment to reduce brain damage following a loss of blood supply, as in cases
78 of sudden cardiac arrest with return of spontaneous circulation (ROSC) (1–4).

79 HRI present on a continuum of pathological states that range from mild to severe (5). If
80 undetected or ineffectively treated, mild HRI can lead to heatstroke, a severe, life-threatening
81 illness (6). Exertional heatstroke (EHS), a consequence of attenuated whole-body heat loss and
82 the inability to dissipate metabolic heat production, can occur while physically active in either
83 temperate or, hot humid conditions (7). Predisposing risk factors include lack of acclimatisation,
84 dehydration, sleep deprivation, low aerobic fitness and diverse biophysical characteristics (6),
85 meaning the onset can be sporadic and unpredictable.

86 CBT cooling is employed within sporting and occupational health settings prior to and between
87 aerobic exercise or firefighting tasks, which have shown to improve performance in heat stress
88 and reduce physiological and, or perceptual strain (8–10). Methods employed to actively cool
89 vary according to setting and application, while HRI treatment is largely dependent upon the
90 duration and extent to which CBT exceeds critical levels (7). Examples of these modalities
91 include whole-body cold water immersion (CWI) (11), ice slurry ingestion (12), pre-prepared
92 ice packs, evaporative techniques or a combination thereof (13). In contrast, early cooling for
93 post-ROSC patients is difficult pre-admission to hospital due to equipment portability and
94 effectiveness (14), while the precise CBT to be targeted for TTM remains controversial (3).

95 Currently, available cooling techniques are either external, non-invasive treatments which
96 provide surface heat exchange, or internal, invasive devices that reduce blood temperature
97 through infused cold saline or nasal spray (15,16). Difficulties thus far have been the design of a
98 device that achieves sufficient and extended cooling non-invasively in the field, pre-admission
99 to the hospital and without use of cooling tanks, refrigeration units, or electrical supply. The
100 CAERvest[®], a chemically powered, easy to activate, endothermic device that covers the torso,
101 upper abdomen and extends onto the neck, purports to overcome these problems.

102 We undertook an initial controlled pilot study in healthy normothermic individuals to establish
103 whether CAERvest[®] prototypes could significantly reduce core and skin temperature effectively
104 over a 60 min period of cooling. Various prototypes were simultaneously assayed to compare
105 efficacy and establish product safety. This testing was also intended to provide data to satisfy
106 regulatory requirements. It was hypothesised there would be no significant difference in core

107 temperature in a defined group of participants within- and between-data collected over the
108 cooling period in any prototype.

109 **2.0 MATERIALS AND METHODS:**

110 **2.1 Participants**

111 Eight moderately active, male participants (mean (M) \pm standard deviation [SD]; age 27 ± 5 years,
112 stature 179 ± 4 cm, nude body mass [NBM] 79.9 ± 1.9 kg, body surface area [BSA] 1.99 ± 0.05 m²,
113 body mass index [BMI] 24.4 ± 0.2 and body fat percentage 16.1 ± 3.8 %) volunteered for the study
114 having provided written informed consent. Male participants were recruited to control for
115 thermoregulation deviation around the menstrual cycle (17). Participants confirmed they were
116 healthy, taking no medication and had no serious medical history or prior cold-related injuries.
117 The study was approved by the Institution's Research Ethics and Governance Committee and
118 conducted in accordance with the Declaration of Helsinki of 1975, as revised in 2013. Participants
119 refrained from caffeine, alcohol consumption and prolonged strenuous activity for 24 h prior to
120 testing. Participants also abstained from food for 2 h before testing and to arrive in a euhydrated
121 state (18).

122 **2.2 Experimental design**

123 Each participant visited the laboratory on four occasions, separated by >72 h to complete the first
124 three CAERvest[®] trials (proof of concept [PoC], prototype 1 [P1] and prototype 2 [P2]), which
125 were counterbalanced using a cross-over design. This then informed the product development
126 for the final CAERvest[®] trial (prototype 3 [P3]), which was completed 21 days after their first
127 visit by all of the participants (Figure 1). Trials were completed in temperate conditions (20°C ,
128 40% relative humidity), with participants wearing only shorts and t-shirt at similar times of the
129 day to minimise circadian rhythm variations (19). Each visit followed the same protocol (Figure
130 2), although the allocated CAERvest[®] prototype changed per trial.

131 **2.3 Physiological measures and equipment**

132 *Body fat* was estimated using skinfold calipers (Harpenden, UK,) across four standard sites (20).
133 Participants provided, in privacy, a fresh mid-flow urine sample which was assessed for
134 osmolality (U_{osm}) (Osmocheck, Vitech Scientific, Japan) and specific gravity (U_{sg}) (hand
135 refractometer, Atago, Japan) to indicate hydration status. Stature and NBM were measured using
136 physician (Detecto scale company Inc., USA) and weighing scales (Adam GFK 150, Equipment
137 Co., UK) respectively, for BMI and BSA calculation (21). Blood pressure (BP) was assessed
138 using an automatic monitor (Boso Medicus PC, Cranlea & Company, UK). *Rectal temperature*
139 (T_{re}) was assessed continuously using a rectal probe (4600 thermometer, Henleys medical
140 supplies, UK) inserted 10 cm past the anal sphincter. Although minor delays to rapid transients
141 are associated with T_{re} when compared with esophageal measurement, the equipment's accuracy
142 is $\pm 0.13^{\circ}\text{C}$ (22). *Heart rate (HR)* (Polar Electro, Finland) monitors were affixed and skin surface

143 telemetry thermistors (U–type connected to Gen II GD38 transmitter, Eltek, UK) were attached
144 to four sites (mid–belly of the pectoralis major, biceps brachii, rectus femoris and gastrocnemius).
145 Data was transmitted wirelessly from a logging device (RX250AL 1000 series wireless squirrel
146 logger, Eltek, UK), which is accurate to $<0.1^{\circ}\text{C}$ (23). *M weighted skin temperature* (T_{skin}) were
147 estimated using the equation of Ramanathan, (24); $M T_{\text{skin}} = 0.3 \times (T_{\text{chest}} + T_{\text{arm}}) + 0.2 \times (T_{\text{thigh}} + T_{\text{calf}})$.
148 Where T_{chest} , T_{arm} , T_{thigh} and T_{calf} are *chest*, *arm*, *thigh* and *calf temperature*, respectively.

149 **2.4 Perceptual measures**

150 Participants were familiarised to the perceptual scales on their first visit. These included *thermal*
151 *sensation (TSS)* on an 8–point scale (0 = *unbearably cold* – 8 = *unbearably hot*) (25); *feeling* on
152 a 10–point scale (+5 = *very good* – –5 = *very bad*) (26); *cold discomfort* on a 10–point scale (0 =
153 *comfortable with no experience of cold* – 10 = *unbearably cold*) (27) and *shivering* on a 4–point
154 scale (0 = *absence* – 3 = *severe*) (28).

155 **2.5 CAERvest[®] devices and development**

156 The CAERvest[®] devices contain a precise quantity of non–toxic chemical blend (developed by
157 BodyChillz, UK) which, when combined with a defined volume of water from an external
158 reservoir, undergoes an endothermic dissolution process and cools for >1 h. Reservoirs were
159 placed in a water–bath (Fischer Scientific DMU19, UK) to control water temperature ($18 \pm 1^{\circ}\text{C}$),
160 as this represented a reasonable storage temperature for a commercial device. The PoC device
161 comprised three separate compartmentalised, dual layer, polyethylene modules filled with blend
162 and activated by 0.8 L of water. One was placed underneath the participant’s back, two were
163 placed across the torso and another smaller module was placed around the neck. A total 4.05 kg
164 of chemical was applied.

165 The subsequent prototypes (P1, P2 and P3) were larger, single module designs intended to target
166 high blood flow regions in neck, axillae and groins and allow for cardiopulmonary resuscitation
167 (CPR), defibrillation or post resuscitation care. The CAERvest[®] are also compatible with the
168 LUCAS[™] and Autopulse[®] chest compression systems. The P1 was the first single module design
169 which covered the torso and groins of the participant and the filling mechanism was as per the
170 PoC. A cellulose matrix was introduced in the P2 along with an incorporated neck section to cool
171 the neck vessels preferentially. A solid non–spill quick disconnect coupling was employed to fill
172 this prototype, with the female attached to the module and male to the reservoir. It was concluded
173 after testing the PoC, P1 and P2 prototypes that the polyethylene material was too rigid and
174 insufficiently elastic in nature. Therefore, a further prototype (P3) as displayed in Figure 3,
175 retained the quick–disconnect coupling for filling and used 150 mm micron polyurethane on the
176 inner surface. Nylon coated polyurethane was adopted on the outer portions of the device to
177 improve insulation for the non–contact surface. The P3 design also removed the sections

178 specifically targeting the neck and groin, which were found to be difficult to position, and
179 increased coverage over the shoulders. The internal channels were redesigned such that fluid
180 entering through the inlet port would push any entrapped air towards newly-introduced one-way
181 valves at the apex of the neck. These valves allowed entrapped air to pass out without causing
182 airlock, fluid loss or points of insulation. The expanding cellulose matrix then caused the device
183 to swell upon fluid introduction and take on a garment-like configuration which improved patient
184 comfort, ensured homogeneity of cooling, minimised movement of the incorporated chemicals
185 in transit and reduced the incidence of cold spots.

186 **2.6 Safety**

187 Signs and symptoms of cold-related injuries were assessed on removal of the CAERvest® device
188 and after the re-warming period. Skin surface was assessed for blistering, oedema and severe
189 erythema, with trial termination if present (zero incidences). Reappraisal of signs and symptoms
190 of cold injury was completed by telephone contact 24 h later.

191 **2.7 Experimental procedures**

192 Hydration status and anthropometric measures were completed on each participant prior to each
193 trial. Temperature and cardiovascular measuring equipment was then attached before a 30 min
194 baseline rest in a supine position. At the end of this, the allocated CAERvest® prototype was
195 applied for 60 min. It was removed early at the participant's request (one incidence at 50 min
196 during the PoC trial), or if T_{re} dropped 1.5°C below resting levels (zero incidences). Cold injury
197 assessments were then completed prior to a re-warming period, where CBT returned naturally,
198 or was aided using extra clothing and light exercise at the participant's discretion. Temperature,
199 cardiovascular and perceptual measures were continuously monitored throughout and recorded
200 at 5 min intervals.

201 **2.8 Safety follow up**

202 Twenty four hours after each trial, follow-up questionnaires and telephone conversations were
203 conducted to account for any adverse effects of cooling (one minor headache).

204 **2.9 Statistical analyses**

205 The trials were an open study of efficacy, assessed by temperature changes over time while using
206 the four CAERvest® prototypes. All data are presented as $M \pm SD$ and were assessed for normality
207 and sphericity prior to statistical analysis. Two way, repeated measure Analysis of Variance
208 (ANOVA) were used to test for differences in temperature, cardiovascular and perceptual
209 responses between and within each trial at 5 min intervals. One way repeated measures ANOVA
210 were used to test for the differences in the lowest point and change (Δ) in temperature and

211 cardiovascular measures within- and between-trials. Where appropriate, Bonferroni adjusted
212 pairwise comparisons were used to identify where differences occurred. Lowest M values and Δ
213 in perceptual scales (non-parametric data) were analysed using a Friedman test, with post-hoc
214 analysis using a Wilcoxon signed-rank test. Data were analysed using SPSS version 20.0, with
215 significance set at $p \leq 0.05$. Effect size for main effects and interactions are presented as partial
216 eta squared (ηp^2), while meaningful differences between related samples during the trials were
217 evaluated using Cohen's d (29). Effect size were categorised as small (0.2), moderate (0.5) and
218 large (0.8). Typical error of measurement (TEM) was calculated from the SD of the M difference
219 during 30 min baseline in T_{re} and T_{skin} between the trials, multiplied by 1 squared, then divided
220 by $\sqrt{2}$ (30) and expressed as a M coefficient variation (CV %). Statistical analysis on resting data
221 within the sample population used within this study presented predefined limits in TEM (CV) of
222 0.20°C (0.5%) for T_{re} and 0.64°C (2.2%) for T_{skin} . TEM were used to demonstrate clinically
223 relevant trends within changes in T_{re} and T_{skin} when investigating the CAERvest[®] devices.

224

225 **3.0 RESULTS:**

226 **3.1 Physical characteristics**

227 Participants arrived in similar physiological states across trials with no differences in preliminary
228 measures (all $p>0.05$) (Table 1), apart from M systolic BP, which was elevated ($F(3,21)=3.23$,
229 $p=0.04$, $\eta^2=0.3$) prior to the PoC trial.

230 **3.2 Baseline measures**

231 No within- or between-participant differences were observed in T_{re} ($F(3,21)=0.48$, $p=0.70$,
232 $\eta^2=0.1$) or T_{skin} ($F(3,21)=0.03$, $p=0.99$, $\eta^2=0.0$) across trials. Nor were differences found in HR
233 ($F(3,21)=0.47$, $p=0.71$, $\eta^2=0.1$) or perceptual measures of TSS ($F(3,21)=0.30$, $p=0.82$, $\eta^2=0.0$),
234 *shivering* ($F(3,21)=1.00$, $p=0.41$, $\eta^2=0.1$), *feeling* ($F(3,21)=1.00$, $p=0.42$, $\eta^2=0.1$), or *cold*
235 *discomfort* ($F(3,21)=0.78$, $p=0.56$, $\eta^2=0.1$) scales (Table 2).

236 **3.3 Cooling measures**

237 **Temperature, cardiovascular and perceptual measures within- and between-CAERvest®** 238 **trials:**

239 A main effect for T_{re} ($F(6,42)=5.35$, $p=0.004$, $\eta^2=0.4$) and T_{skin} ($F(6,36)=3.46$, $p=0.01$, $\eta^2=0.4$)
240 occurred in all four trials, with significant pre-to-post reductions (Figure 4 and Table 3). On one
241 occasion the PoC was removed at 50 min upon the participant's request. ΔT_{re} was significantly
242 greater ($p=0.047$) during the PoC trial ($-0.36\pm 0.18^\circ\text{C}$, $d=1$) compared to the P1 ($-0.17\pm 0.13^\circ\text{C}$,
243 $d=0.9$). Moreover, during the P3 trial the ΔT_{skin} ($-2.47\pm 0.82^\circ\text{C}$, $p=0.001$, $d=1$) were significantly
244 greater than the P2 trial ($-0.98\pm 0.93^\circ\text{C}$, $d=0.7$) (Table 3).

245 There was a significantly larger ΔT_{re} ($F(7,49)=5.33$, $p=0.00$, $\eta^2=0.4$) during the CAERvest®
246 cooling period compared to the ΔT_{re} during baseline rest. This was found within the PoC ($p=0.01$)
247 and P3 ($p=0.01$) trials, but not the P1 ($p=0.45$) or P2 ($p=0.28$) trials. A similar interaction effect
248 was found for ΔT_{skin} ($F(7,49)=37.24$, $p=0.00$, $\eta^2=0.8$) within the PoC ($p=0.02$), P1 ($p=0.01$) and
249 P3 ($p=0.00$) trials, but not for P2 ($p=0.09$).

250 An interaction effect occurred between time and CAERvest® in *shivering* ($F(36,108)=1.55$,
251 $p=0.04$, $\eta^2=0.3$) and *cold discomfort* ($F(36,108)=2.345$, $p=0.001$, $\eta^2=0.4$) scales. *Shivering*
252 ($Z=-2.04$, $p=0.04$) and *cold discomfort* ($Z=-2.23$, $p=0.03$) scales were significantly greater during
253 the PoC (1 ± 1 and 5 ± 2 , respectively) compared to the P1 trial (0 ± 0 and 4 ± 2 , respectively). *Cold*
254 *discomfort* ($Z=-2.13$, $p=0.03$) scales were also higher during the P3 (5 ± 3) compared to P2 trial
255 (3 ± 2) (Table 4).

256 An interaction effect between time and CAERvest[®] occurred in T_{re} ($F(36,216)=1.91$, $p=0.003$,
257 $\eta p^2=0.2$) and T_{skin} ($F(36,72)=2.60$, $p=0.001$, $\eta p^2=0.6$), as displayed within Figure 4 and 5.

258 No interactions were present in HR ($F(36,144)=0.36$, $p=1.00$, $\eta p^2=0.1$), TSS ($F(36,108)=1.497$,
259 $p=0.06$, $\eta p^2=0.3$), or *feeling* ($F(36,108)=1.24$, $p=0.20$, $\eta p^2=0.3$) scales in the same period.

260 **3.4 Device safety analysis**

261 There was no evidence of cold-related injuries across all four CAERvest[®] prototypes. The only
262 symptoms resulting from the trials were mild skin paleness on removal of the device and one
263 reported headache within 6 h of PoC removal. Neither of these symptoms were considered to
264 represent a serious adverse event. Headaches have been recorded in other cooling garment studies
265 (31).

266

267 **4.0 DISCUSSION**

268 The aim of this study was to inform the development and investigate the safety and efficacy of a
269 series of CAERvest[®] prototypes. Therefore, the study was designed to examine the null
270 hypothesis, that there would be no significant difference in CBT in a defined group of participants
271 during the cooling period in any prototype. We found significant reductions in T_{re} and T_{skin} with
272 each device. The PoC and P3 CAERvest[®] were found to provide greater temperature reductions
273 than the P1 and P2, suggesting improved design. It is postulated that in the PoC this may be
274 because of increased mass and in the P3, despite reduced chemical mass, improved surface area
275 coverage and thermal coupling to the skin. We found no evidence of important cold-related signs
276 or symptoms from the CAERvest[®] devices during the cooling period, or in the subsequent 24 h.
277 As the CAERvest[®] was being developed during the study, no comparisons were made with other
278 similar devices, although future studies will address this.

279 **4.1 Comparisons to other cooling modalities**

280 Previous studies investigating surface cooling devices have reported effective (32–39) and
281 ineffective (40–46) physiological responses in athletic performance, and thermoregulatory strain
282 reductions within hyperthermic individuals. As EHS treatment requires a rapid cooling rate of
283 $0.1\text{--}0.2^{\circ}\text{C}\cdot\text{min}^{-1}$ (47), Lopez et al. (44), DeMartini et al. (45) and Flouris et al. (11) suggest the
284 continued use of CWI as the standard for hyperthermic individuals, with reported cooling rates
285 of $0.1\text{--}0.35^{\circ}\text{C}\cdot\text{min}^{-1}$. This is opposed to the less effective treatment of ice-wet towels
286 ($0.11^{\circ}\text{C}\cdot\text{min}^{-1}$), ice packs ($0.03^{\circ}\text{C}\cdot\text{min}^{-1}$) and fans ($0.02^{\circ}\text{C}\cdot\text{min}^{-1}$) (48). Within this study the 60
287 min cooling rate for PoC and P3 were $0.01^{\circ}\text{C}\cdot\text{min}^{-1}$, while they were $0.003^{\circ}\text{C}\cdot\text{min}^{-1}$ for the P1
288 and P2, however, the authors acknowledge the normothermic population tested and associated
289 study limitations which are later discussed, although there still remains distinct advantages of a
290 portable, on-site method.

291 Further, other pre- and in-hospital surface cooling systems which have been used upon
292 hyperthermic or cardiac arrest casualties, include the CritiCool (Curewrap[™], MTRE, Yavne,
293 Israel), Blanketrol III (Kool-Kit[®], Cincinnati Sub-Zero, OH, USA), EMCOOLS (Flex.Pad[®])
294 and Artic Sun[®] (Medivance, Louisville, CO, USA) have reported cooling rates of $1.5\text{--}3.5^{\circ}\text{C}\cdot\text{h}^{-1}$
295 (49,50). While InnerCool STX (Phillips, Best, Netherlands) and Thermogard XP[®] (ZOLL)
296 intravascular systems report $2\text{--}5^{\circ}\text{C}\cdot\text{h}^{-1}$ (49). Finally, the intranasal device, RhinoChill[®]
297 (BeneChill, CA, USA) reports 1.75°C reductions in the first hour of cooling (16,51). However,
298 the large variation in cooling suggests product design and function play a key role in achieving
299 clinically important reductions. Although, it is recognised that disparity may also result from
300 alternate methodologies, cooling modalities, aerobic activity and the use of hyperthermic or
301 cardiac arrest patients. These differences make it very difficult to compare across studies. There

302 are however, disadvantages associated with these pre-hospital methods, including trivial benefits
303 of evaporative fanning or misting (52), unconscious individuals are unable to ingest ice slurries,
304 powered refrigerator requirements and impracticality of CWI, thus failing to provide a portable
305 or flexible solution. Moreover, infusing cold saline intravenously is invasive, requires specialist
306 training and causes additional stress to the circulatory system, often with deleterious effects
307 (53,54). The in-hospital surface cooling devices are effective, but require electrical supply,
308 refrigeration and are sometimes restricted to intensive care units. Finally, the intranasal device,
309 can only be used on unconscious individuals and has large consumable costs (55).

310 **4.2 Physiological responses**

311 T_{re} was shown to reduce significantly pre-to-post while using all four CAERvest® designs, with
312 the largest reported reductions observed in the PoC ($-0.36 \pm 0.18^\circ\text{C}$) and P3 ($-0.36 \pm 0.22^\circ\text{C}$) trials.
313 Although the PoC implemented a larger surface area of cooling (56), there were no differences
314 compared with the P3 CAERvest®. It is suggested the large range in T_{re} reductions during the
315 PoC ($-0.12 - -0.64^\circ\text{C}$), P1 ($-0.12 - -0.41^\circ\text{C}$), P2 ($-0.07 - -0.41^\circ\text{C}$) and P3 ($-0.07 - -0.65^\circ\text{C}$)
316 trials highlight inter-individual variances within the sample population. Significantly greater ΔT_{re}
317 and ΔT_{skin} were observed during the cooling period compared to the baseline resting period during
318 the PoC and P3 trials, as opposed to no difference during the P1 and P2. Thus, highlighting the
319 greater effect of CBT cooling compared to a no-cooling control state.

320 The observed T_{skin} reductions ($2-3^\circ\text{C}$) are in line with previously cooled hyperthermic (44) and
321 normothermic (37) individuals in warm conditions. T_{skin} during the P3 trial was significantly
322 lower in the latter stages of the cooling period compared to the PoC and P2 trial, suggesting
323 effective and prolonged cooling. Reportedly, optimal vasodilation, core to skin thermal gradient
324 and therefore, a greater heat flux occurs at $T_{skin} \sim 33-35^\circ\text{C}$ (32). T_{skin} in this study reduced to
325 $<33^\circ\text{C}$ in all four trials. Although, this may have appeared as chest and tricep skin thermistors
326 were placed underneath the CAERvest® devices, leading to larger magnitudes of $M T_{skin}$ declines,
327 as similarly observed by Teunissen et al. (57).

328 While the authors acknowledge the temperature reductions within the study are comparatively
329 modest, it is suggested the limited reductions were observed because the study was performed in
330 a young, asymptomatic healthy population of moderate fitness levels. These individuals may
331 present characteristics similar to those heat-acclimatised, such as lower internal temperature set
332 points (58) and modified thermoregulatory mechanisms, with improved capacity for
333 vasoconstriction (59). Therefore, participants may have been particularly resilient to an external
334 cold induced stimulus and, subsequently, more effective in defending their CBT through
335 homeostasis. Those with predisposing risk factors, exertional heat illnesses or symptomatic
336 clinical populations are expected to be less resistant to cooling due to hypothalamic dysfunction

337 and CBT regulation disruption after the traumatic event occurs (6,60–65). Extending the
338 evaluation of the CAERvest® to other symptomatic populations warrants further investigation.

339 **4.3 Perceptual responses**

340 While perceptual measures are important for investigating cooling interventions (57), most
341 studies use perceived comfort to assess efficacy prior to and during physical activity in an attempt
342 to enhance performance (12,66), or reduce physiological strain (57). As expected, *TSS* decreased
343 during cooling in all four trials, although no interaction effect occurred. Nor were differences
344 observed in *feeling* scale within- or between-trials, suggesting the PoC and P3 CAERvest® did
345 not make participants feel worse over time, although they felt colder and presented minor
346 shivering responses.

347 **4.4 Limitations and future directions**

348 Aforementioned, the study used healthy, normothermic individuals as opposed to clinical or
349 hyperthermic populations, who are known to be more susceptible to external cold stimulus.
350 Therefore, caution should be used if extending the results of this study to the general population.
351 An additional limitation includes no control trial, although each cooling period was compared
352 against prior resting measures within- and between-trials. Directions for future CAERvest®
353 investigations will include evaluation of product efficacy across a range of exercise-induced
354 hyperthermic individuals, in addition to comparisons against other cooling modalities and
355 normothermic post-cardiac arrest populations.

356 **5.0 CONCLUSION**

357 This study observed reductions in core and skin temperature without incidence of cold injury in
358 the proof of concept and latter CAERvest® prototype design. The latest P3 CAERvest® is a
359 portable, non-powered, easy-to-use device, which may offer an alternative on-site or pre-
360 hospital strategy for those suffering from HRI or ischemic related events, as a single or combined
361 approach with other modalities, to induce rapid cooling without the prior preparation required.
362 However, further research is warranted in controlled laboratory and field-based settings to
363 continue the evaluation and development of this technology.

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366 also goes to Tom Howes, senior technician, for his technical support throughout.

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6.1 CONFLICT OF INTEREST AND FUNDING

Steve Tocker, Dr. Rowland Cottingham and William Simpson, listed as co-authors, are associated with the company that commissioned the product testing, BodyChillz. These individuals were not involved in the data collection or statistical analyses, their involvement was limited to demonstration of CAERvest[®] prototypes, familiarisation of the study team and the review of this manuscript.

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544 **FIGURE TITLES**

545 Figure 1:

546 Schematic of experimental design. Prototype 3 (P3) was introduced after the proof of concept (PoC),
547 prototype 1 (P1) and prototype (P2) trials, due to refinements in design following analysis and therefore,
548 were not part of the randomization.

549 Note: The full colour version of this figure is available online.

550 Figure 2:

551 Schematic of experimental design.

- 552 A- Body mass, stature, body surface area, body mass index, hydration status, blood pressure.
553 B- Physiological (*rectal temperature, skin temperature and heart rate*) and perceptual (*thermal
554 sensation, cold discomfort, feeling, shivering*) measures monitored continuously and recorded
555 every 5 min.
556 C- Medical inspection for any associated cold related injuries.

557 Note: PoC = proof of concept, P1 = prototype 1, P2 = prototype 2 and P3 = prototype 3.

558 Figure 3.

559 Photo of prototype 3 on a participant.

560 Note: The full colour version of this figure is available online.

561 Figure 4.

562 *Mean rectal temperature* changes over the cooling period. Significance ($p<0.05$) is denoted by ‡
563 between PoC and P1, * between P3 and P1.

564 Note: PoC = proof of concept, P1 = prototype 1, P2 = prototype 2 and P3 = prototype 3.

565 Figure 5.

566 *Mean skin temperature* changes over the cooling period. Significance ($p<0.05$) is denoted by * between
567 P3 and P2, and ‡ between P3 and PoC.

568 Note: PoC = proof of concept, P1 = prototype 1, P2 = prototype 2 and P3 = prototype 3.

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Table 1. Mean (*SD*) preliminary health measures on the arrival to each trial.

Measure	Trial			
	PoC	P1	P2	P3
NBM (kg)	81.1 ± 15.2	81.2 ± 15.1	76.1 ± 10.2	80.0 ± 15.7
BMI	24.6 ± 4.0	24.6 ± 3.9	23.1 ± 2.8	24.2 ± 3.9
BSA (m ²)	2.01 ± 0.19	2.01 ± 0.19	1.96 ± 0.14	2.00 ± 0.20
Systolic BP (mmHg)	148 ± 18*	144 ± 17	135 ± 5	134 ± 10
Diastolic BP (mmHg)	81 ± 12	79 ± 5	81 ± 6	79 ± 6
U _{osm} (mOsmol·kg ⁻¹ H ₂ O)	491 ± 104	524 ± 228	450 ± 157	389 ± 213
U _{sg}	1.013 ± 0.004	1.014 ± 0.008	1.010 ± 0.005	1.010 ± 0.006

Note: * denotes significant difference between other trials, where $p < 0.05$. PoC = proof of concept, P1 = prototype 1, P2 = prototype 2 and P3 = prototype 3. BP = blood pressure, BMI = body mass index, BSA = body surface area, NBM = nude body mass, U_{osm} = urine osmolality, U_{sg} = urine specific gravity.

Table 2. Mean (*SD*) and change in baseline physiological and perceptual measures.

Measure		Trial			
		PoC	P1	P2	P3
T_{re} (°C)	<i>M</i>	37.11 ± 0.29	37.10 ± 0.26	37.10 ± 0.27	37.18 ± 0.26
	Δ	-0.13 ± 0.10	-0.14 ± 0.13	-0.09 ± 0.10	-0.11 ± 0.07
T_{skin} (°C)	<i>M</i>	31.29 ± 1.01	31.14 ± 1.02	30.92 ± 1.43	30.97 ± 1.18
	Δ	1.08 ± 0.38	1.11 ± 0.76	1.04 ± 0.60	1.04 ± 0.45
<i>HR</i> (bpm)	<i>M</i>	63 ± 8	61 ± 9	64 ± 7	63 ± 9
	Δ	-1 ± 6	-2 ± 7	-1 ± 8	-1 ± 4
<i>TSS</i>	<i>M</i>	4 ± 1	4 ± 1	4 ± 0	4 ± 1
	Δ	0 ± 0	0 ± 0	0 ± 0	0 ± 0
<i>Shivering</i>	<i>M</i>	0 ± 0	0 ± 0	0 ± 0	0 ± 0
	Δ	0 ± 0	0 ± 0	0 ± 0	0 ± 0
<i>Feeling</i>	<i>M</i>	2 ± 2	3 ± 2	2 ± 2	2 ± 2
	Δ	0 ± 0	0 ± 0	0 ± 0	0 ± 0
<i>Cold discomfort</i>	<i>M</i>	1 ± 1	0 ± 1	0 ± 0	0 ± 1
	Δ	0 ± 0	0 ± 0	0 ± 0	0 ± 1

Note: PoC = proof of concept, P1 = prototype 1, P2 = prototype 2 and P3 = prototype 3. Δ = change, *HR* = heart rate, *M* = mean, T_{re} = core temperature, T_{skin} = skin temperature, and *TSS* = thermal sensation scale.

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Table 3. Pre–post mean (*SD*) changes in physiological measures during cooling.

Measure	Trial	Time (min)		
		0 min	60 min	Δ 0–60
T_{re} (°C)	PoC	37.04 ± 0.29	36.68 ± 0.42	−0.36 ± 0.18* ⁺
	P1	37.03 ± 0.23	36.86 ± 0.26	−0.17 ± 0.13*
	P2	37.06 ± 0.27	36.87 ± 0.24	−0.19 ± 0.17*
	P3	37.12 ± 0.23	36.76 ± 0.28	−0.36 ± 0.22*
T_{skin} (°C)	PoC	31.76 ± 1.12	30.18 ± 1.38	−1.55 ± 0.97*
	P1	31.59 ± 0.95	29.39 ± 0.62	−2.20 ± 1.04*
	P2	31.33 ± 1.50	30.35 ± 1.22	−0.98 ± 0.93*
	P3	31.42 ± 1.14	28.95 ± 1.10	−2.47 ± 0.82* [†]
<i>HR</i> (bpm)	PoC	63 ± 10	56 ± 9	−7 ± 12
	P1	60 ± 8	53 ± 7	−7 ± 3
	P2	65 ± 6	60 ± 6	−5 ± 4
	P3	63 ± 9	56 ± 8	−7 ± 8

Note: * denotes significant ($p < 0.05$) difference within trials for pre to post changes, ⁺ between PoC and P1, and [†] between P3 and P2 change. PoC = proof of concept, P1 = prototype 1, P2 = prototype 2 and P3 = prototype 3. Δ = change, T_{re} = core temperature and T_{skin} = skin temperature.

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Table 4. Pre–post mean (*SD*) changes in perceptual measures during cooling.

Measure	Trial	Time (min)		
		0 min	60 min	Δ 0–60
<i>TSS</i>	PoC	4 ± 1	2 ± 1	-2 ± 1*
	P1	4 ± 1	3 ± 1	-1 ± 1*
	P2	4 ± 0	3 ± 1	-1 ± 1*
	P3	4 ± 1	2 ± 1	-2 ± 1*
<i>Shivering</i>	PoC	0 ± 0	1 ± 1	1 ± 1 [§]
	P1	0 ± 0	0 ± 0	0 ± 0
	P2	0 ± 0	0 ± 0	0 ± 0
	P3	0 ± 0	1 ± 1	1 ± 1
<i>Feeling</i>	PoC	2 ± 2	0 ± 3	-2 ± 2
	P1	3 ± 2	1 ± 3	-1 ± 2
	P2	2 ± 2	1 ± 3	-1 ± 1
	P3	2 ± 2	0 ± 3	-1 ± 2
<i>Cold discomfort</i>	PoC	1 ± 1	4 ± 2	4 ± 2*
	P1	0 ± 1	3 ± 3	2 ± 3*
	P2	0 ± 0	3 ± 2	3 ± 2*
	P3	1 ± 1	5 ± 2	4 ± 2*

Note: * denotes significant ($p < 0.05$) difference within trials for pre to post changes, [§] between P1 and P2. PoC = proof of concept, P1 = prototype 1, P2 = prototype 2 and P3 = prototype 3. Δ = change and *TSS* = *thermal sensation scale*.

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PoC



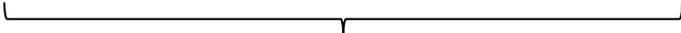
P1



P2



P3



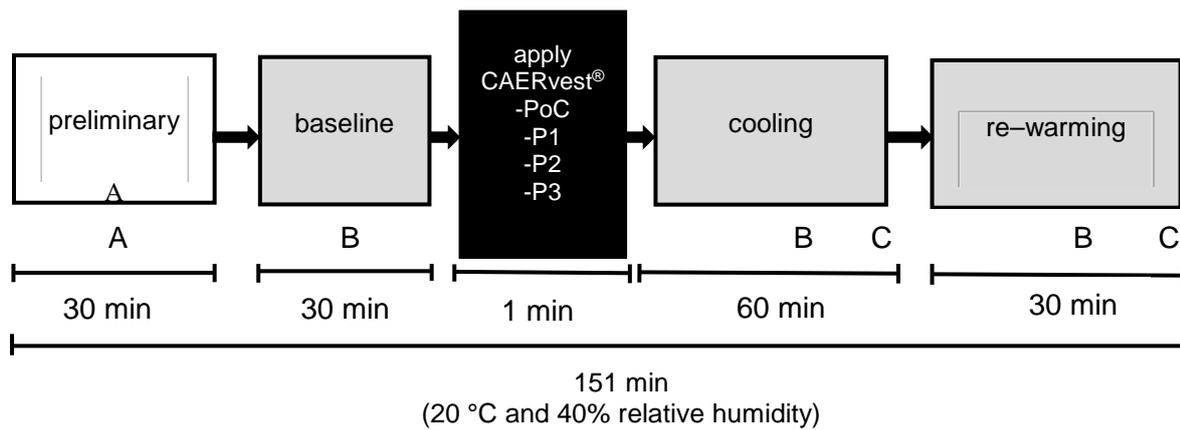
counterbalanced order



final trial

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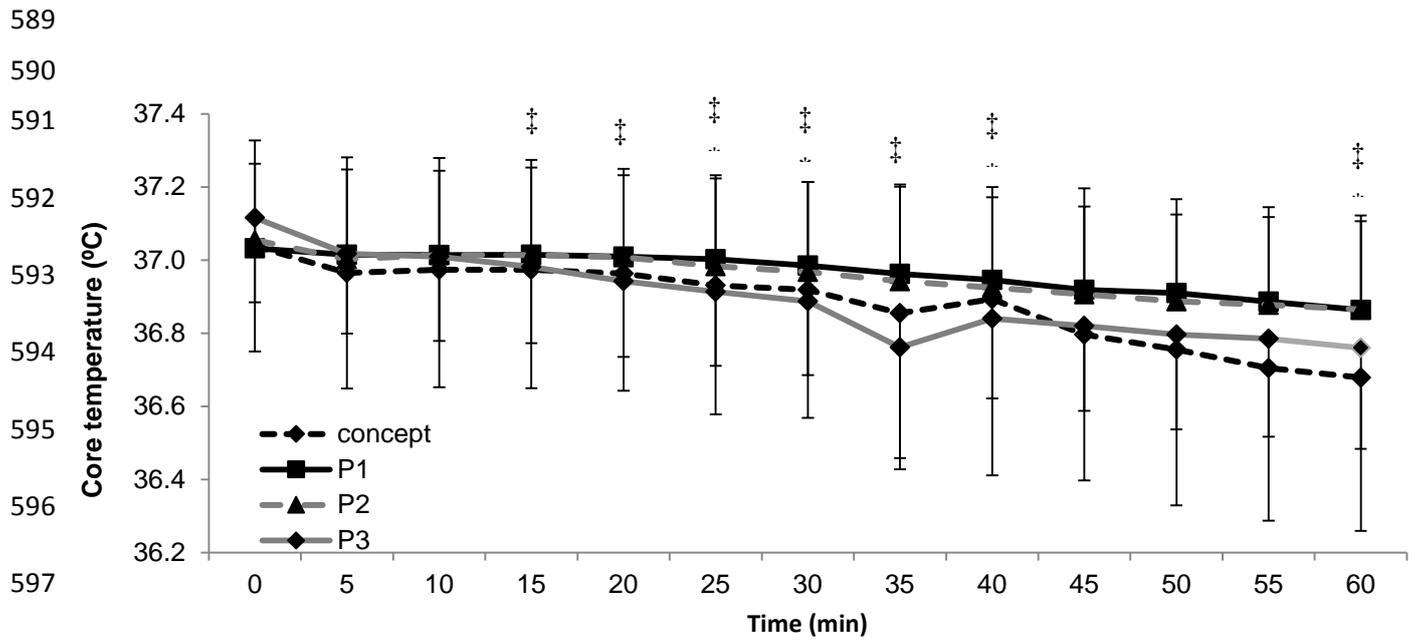
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